

4805 (3/11)

CBSOLLTE       ZS       C.084 [ .000]       12.000]       14.83 [ .000]       14.83 [ .000]       12.000]       12.000]       12.000]       12.000]       12.000]       12.000]       12.000]       12.000]       12.000]       12.000]       12.000]       12.000]       12.000]       12.000]       12.000]       12.000]       12.000]       14.83 [ .000]       10.000]       146309-         SUPERCEDED       SUPERCEDED       SUPERCEDED       1.484 [ .000]       4       10.000]       146309-5       12.000]       12.000]       4       10.000       146309-6         SUPERCEDED       SUPERCEDED       SUPERCEDED       SUPERCEDED       1.484 [ .000]       4       10.000       146309-7       3       12.000]       4       10.000       146309-7         SUPERCEDED       SUPERCEDED       SUPERCEDED       SUPERCEDED       SUPERCEDED       3       [ .000]       7.21       5.000]       3       8       -146309-7         SUPERCEDED       SUPERCEDED       SUPERCEDED       SUPERCEDED       SUPERCEDED       12.000]       1       4       146309-7         SUPERCEDED       SUPERCEDED       SUPERCEDED       SUPERCEDED       SUPERCEDED       SUPERCEDED       12.000]       1       4       146309-7							DIMENSIONS: mm [INCHES]	0 PLC = 1 PLC = 2 PLC = 3 PLC =		SIZE	GH TEMPERATURE, RIG	MOD II, BREAKAWAY, HT ANGLE, DOUBLE ROW /.025 SQUARE POSTS Restrict
A         Right Product         FA         A <tha< th="">         A         A         &lt;</tha<>						PUSITIONS	THIS DRAWING IS A	CONTROLLED	DOCUMENT. CHK CHK CHK CHK CHK CHK CHK CHK	1-6-95		TE Connectivity
CESOLE E         A         SUB_T #5005         -14         SUB_T #5005         S	N				A		PART NUMBER			A		PART NUMBER
CHESCIL E         CHESCIL FE         CHESCIL			2.13		0			$\overline{\wedge}$	2.13 -	0		
A         North         Solid         Solid <thsolid< th="">         Solid         Sol</thsolid<>			_ 4.67 _	_ 2.54 _	1			$\wedge$	_ 4.67 _ 2.54 _	1		146309-
A         State         State <thstate< th="">         State         Stat</thstate<>	ORSOLFTE	$\wedge$	7.21	5.08				$\wedge$	[7.21, 5.08]			
A         C1212         S250         50         60         0         -(-6300         A         C362         C360         C4         (1000)           C380         T         C362         S260         18         C7         C6         E-(-6300-0)         A         C362         C7         C4         C4 <thc4< th="">         C4         <thc4< th=""> <thc4< th=""> <thc4< th="">        &lt;</thc4<></thc4<></thc4<></thc4<>	SUPERCEDED	$\wedge$	_ 9.75 _					$\overline{\wedge}$	$\begin{bmatrix} .+0+] \\ .400 \end{bmatrix}$			146309-
A         B         AC         M-1000000         AC         B         AC         M-1000000         AC         B         AC         M-1000000         AC         B         AC         M-1000000         AC         AC         M-10000000         AC         AC         M-100000000000         AC         AC         M-1000000000000000000000000000000000000		$\wedge$	12.29	_10.16_				$\overline{\underline{3}}$	12.29 10.16			
●         ●	$\bigwedge$	$\wedge$	_14.83_	12.70				<u> </u>				
A         12.82         28.82         34         46         4-1416 (28-2)         12.82         28.85         35         76         3-142329           CBSCITTF         A         12.82         28.85         32         72         2         146205-8         2         28.85         35         76         -3-142329           A         12.82         28.85         32.87         72         2         146203-8         2         28.85         35         77         -3-142329           A         12.82         28.85         32.85         72         2         146203-6         2         28.85         35         72         3         146329           A         12.88         28.85         22.85         22         66         2         146129-4         3         356         33         56         -3-146299           A         12.85         22.85         12         66         2         146129-4         358         33         56         -3-144299           CBSCLTIT         A         12.85         22.85         12         66         2         146129-4         358         33         56         1-144929           CBSCLTIT         A		$\wedge$	784] _ 17.37	_15.24_	,			$\wedge$		·		
A         Units         Parts         53         66         2 * 4 200 - 0         Count         State         State <th< td=""><td>00000000</td><td><math>\wedge</math></td><td>[ .884] _19.91_</td><td>[ .800] 17.78</td><td></td><td></td><td></td><td><math>\overline{\wedge}</math></td><td>.884 .800</td><td></td><td></td><td></td></th<>	00000000	$\wedge$	[ .884] _19.91_	[ .800] 17.78				$\overline{\wedge}$	.884 .800			
A         Constraint         See Set Set Set Set Set Set Set Set Set			984] 22.45	900 20.32	-			$\wedge$	984900_ 22.4520.32 _			
A         IC: 10: 10: 10: 10: 10: 10: 10: 10: 10: 10			[1.084] _24.99_	[1.000] _22.86_				$\overline{\wedge}$	[1.084][1.000] _24.9922.86_			
A         X = 4         X = 5         X = 6         A = 1/4504-0         A = 1/2522         X = 5 <thx 5<="" =="" th=""> <thx 5<="" =="" th=""></thx></thx>		$\frac{5}{5}$	[1.184] 27.53	[1.100] 25.40				$\overline{3}$	27.53 25.40			
A         Correct         State         S		$\frac{5}{5}$	[1.284] _30.07_	[1.200] _27.94_				$\overline{3}$	[1.284][1.200]			
A       10110       20005       39       20       3-45309-0       A       12.12       29.85       29       20       4-45309         DESO_FITE       A       20.23       34       76       3-74       2-45309       38       78       74       2-45309         A       20.24       20.26       37       76       3-74       2-45309       A       20.24       20.25       37       76       3-74 <td></td> <td><u></u></td> <td>[1.384] 32.61</td> <td>[1.300] 30.48</td> <td></td> <td></td> <td></td> <td></td> <td>[1.384][1.300]</td> <td></td> <td></td> <td></td>		<u></u>	[1.384] 32.61	[1.300] 30.48					[1.384][1.300]			
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $		<u>/5</u>	[1.484]	[1.400]				3	[1.484][1.400]			
$A = \begin{bmatrix} 3 & 3 & 3 & 3 & 3 & 3 & 3 & 3 & 3 & 3$		<u>/5</u>	[1.584]	[1.500]					[1.584][1.500]			
A       13,934       33,06       39       80       9-115309-0       A       13,92       13,02       13,02       13,02       13,02       13,02       14       44       54,14509       54       14,000       8       13,02       14,02       14,02       13,02       14,02       14,02       14,02       14,02       14,02       14,02       14,02       14,02       14,02       14,02		<u></u> ^5	[1.684]	[1.600]				3	[1.684][1.600]			
A       IC I D       99332 (10) - 10       35       50       9-110309-0 (10) - 0       A       30911-3000 (10) - 0       39       30       1-110309 (10) - 0         DBSC_ETE       A       10000-1 (10) - 0       31000-1 (10) - 0       <	$\angle 6 $	5	[1.784]	[1.700]	17	36	6-146309-8	3	[1.784][1.700]	17	36	_1_146309
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $		5	[1.884]	[1.800]	18	38	6-146309-9	3	[1.884][1.800]	18	38	1-146309
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $		5	[1.984]	[1.900]	19	40	7-146309-0	3	[1.984][1.900]	19	40	-2-146309
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		5	52.93 [2.084]	50.80 [2.000]	20	42	7-146309-1	$\overline{3}$	[2.084][2.000]	20	42	-2-146309
A         3         3         98         3         96         9-1/15309-0         A         13/162         39/26         39         50         4-146308           DBSOLETE         A         33/84         33/82         33/82         38/84         38/		$\overline{\wedge}$	55.47 [2.184]	<u>53.34</u> [2.100]	21	44	7-146309-2		55.47 53.34 [2.184][2.100]	21	44	-2-146309
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $		$\overline{\wedge}$	58.01	_55.88_	22	46	7-146309-3	$\overline{3}$	58.01_55.88_	22	46	-2-146309
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $		$\overline{\wedge}$	60.55		23	48	7-146309-4		60.55 58.42	23	48	-2-146309
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $			63.09	_60.96_	24	50	7-146309-5	$\overline{ 3}$	63.09 60.96	24	50	-2-146309
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $		$\overline{\wedge}$	65.63	63.5	25	52	7-146309-6	$\overline{)}$	65.63 63.5	25	52	2-146309
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $		$\frac{25}{5}$	68.17	_66.04 _	26	54	7-146309-7	$\overline{)}$	68.17_66.04	26	54	2-146309
$\begin{array}{c c c c c c c c c c c c c c c c c c c $		$\frac{25}{2}$	70.71	_68.58_				$\overline{3}$	_ 70.71_ 68.58_			
$\begin{array}{c c c c c c c c c c c c c c c c c c c $		$\frac{\sqrt{5}}{\sqrt{5}}$	73.25	71.12				<u> </u>				
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\angle 6 $ –	$\frac{5}{1}$	75.79	_73.66_				$\overline{3}$	_ 75.79 73.66 _			
Image: Section of the section of th			[3.184] 78.33	[3.100]				$\wedge$				
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	OBSOLEIE	$\frac{5}{5}$	[3.284]	[3.200]				$\overline{3}$				
Image: Second state of the second s		5	[3.384]					3				
$\begin{array}{c c c c c c c c c c c c c c c c c c c $			[3.484]	[3.400]				3				
$\begin{array}{c c c c c c c c c c c c c c c c c c c $			[3.584]	[3.500]				3	3.584 3.500			
101.19       99.06       39       80       9-146309-0       101.19       99.06       39       80       4-146309         5       [3.984][3.900]       39       80       9-146309-0       3       [3.984][3.900]       39       80       4-146309         6       98.65       96.52       38       78       8-146309-9       3       [3.884][3.800]       38       78       -3-146309         0       96.11       93.98       37       76       8-146309-8       3       [96.11]       93.98       37       76       -3-146309         0       96.11       93.98       37       76       8-146309-8       3       [3.784][3.700]       37       76       -3-146309	6	5	[3.684]	[3.600]			8-146309-7	3	3.684 3.600			_3_146309
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	JBSOLETE	5	[3.784]	[3.700]	37	76	8-146309-8	3		37	76	-3-146309
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		$\sqrt{5}$	[3.884]	[3.800]	38	78	8-146309-9	$\overline{3}$		38	78	-3-146309
		$\sqrt{5}$	[3.984]		39	80	9-146309-0	$\overline{3}$		39	80	4-146309
	_	A	1101 19	99.06				Λ				

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REVISIONS

DESCRIPTION

B REVISED PER ECO-14-000260

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