

Boost to battery evaluation kit

TLD5098EP

About this document

Product description

The TLD5098EP is an AEC qualified DC-DC boost controller, especially designed to drive LEDs.

- Built-in diagnosis and protection features
- Designed to support multiple topologies such as Boost, Buck, Buck-Boost, SEPIC and Flyback

Scope and purpose

Scope of this user manual is to provide instructions on the usage of TLD5098EP boost to battery evaluation board.

Intended audience

This document is intended for engineers who need to perform measurements and check performances with TLD5098EP boost to battery evaluation board.

Table of contents

	About this document	1
	Table of contents	1
1	Description	2
2	Quick start procedure	4
3	Current adjustment	5
4	Power derating (battery dependent current)	6
5	Cold crank survival circuit	7
6	Schematics	8
7	PCB layout	11
8	Bill of material	12
9	Efficiency measurements	14
10	Maximizing efficiency	15
11	Minimizing EM emissions	16
12	Revision history	17
	Disclaimer	18

1 Description

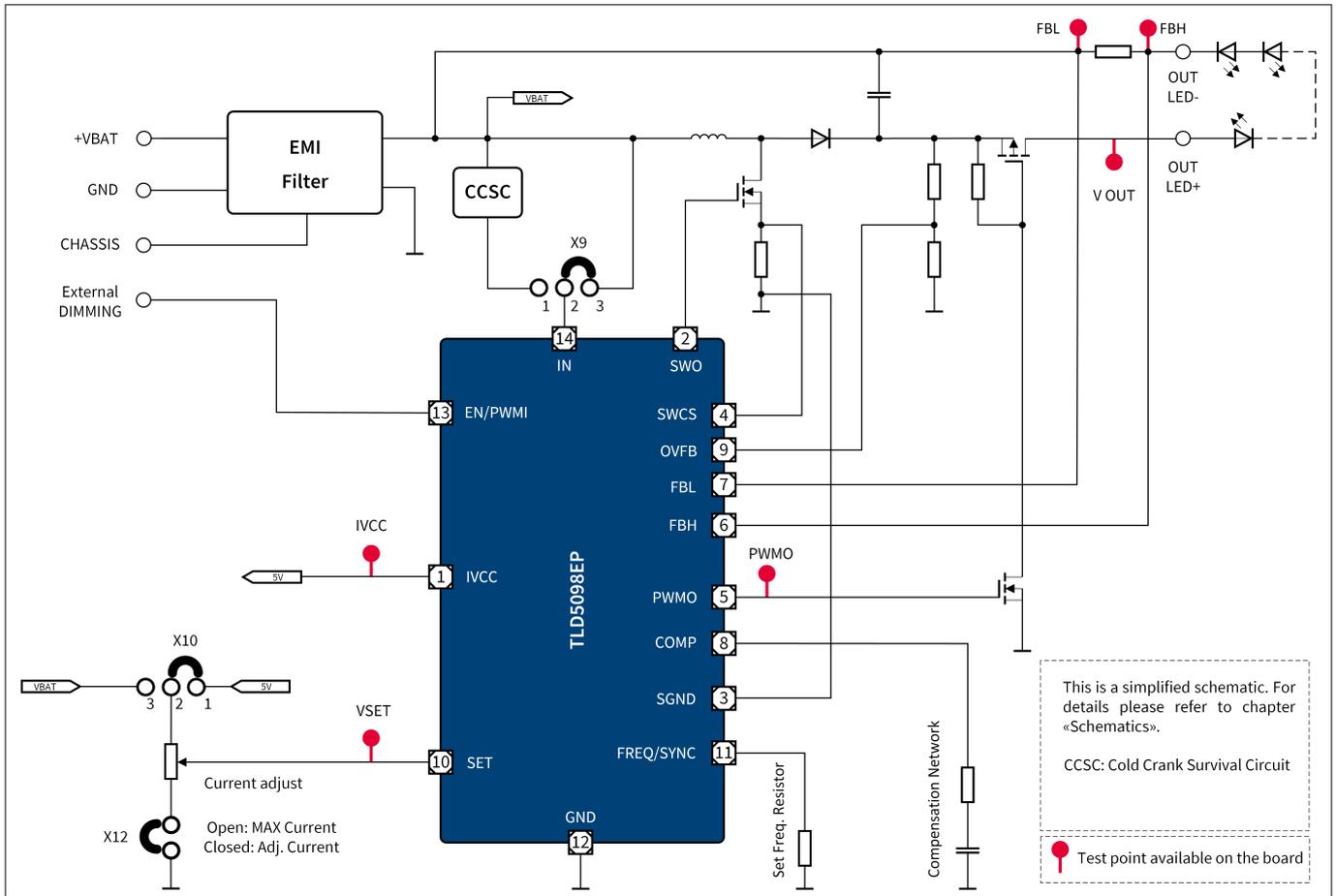


Figure 2 Simplified schematic

Table 1 Performance summary

Parameter	Conditions	Value
Input supply voltage	Jumper X9 in position 2-3 (CCSC deactivated) Parameter degradation below 6.5 V	8 V to 27 V (Down to 6.5 V for less than 2 s)
Input supply voltage	Jumper X9 in position 1-2 (CCSC active)	8 V to 27 V (Down to 3.0 V for less than 2 s)
Output current	Jumper X12 open	1 A
Switching frequency	$V_{IN} = 13.2 V$	400 kHz
Efficiency	Measured with 7 white standard LED 3 V @ 1 A output current	> 85%
Output voltage range	Output voltage related to positive input	16 V to 23 V
Output overvoltage protection	Output voltage related to ground	59 V

2 Quick start procedure

2 Quick start procedure

The default configuration of the board has all additional features disabled. In this configuration the output current cannot be adjusted. The PWM signal has to be applied as digital signal on X18 (max. 45 V).

Jumpers are populated as follows:

Jumper number	Condition	Meaning
X9	Close 2-3	Disable CCSC
X10	Close 2-1	Disable battery dependent current

The default configuration is depicted below:

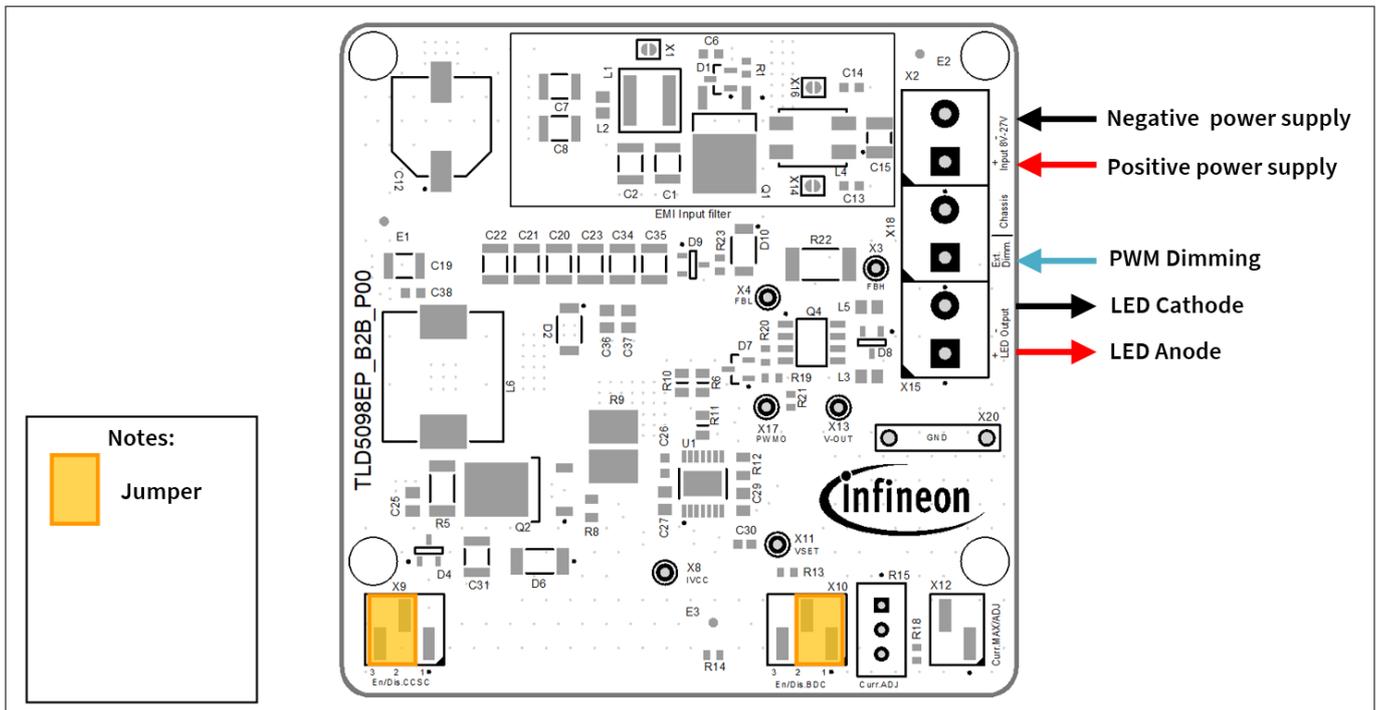


Figure 3 Default configuration of the board

3 Current adjustment

3 Current adjustment

The output current adjustment can be performed by changing the value of trimmer R15 with a screwdriver, when X10 is closed in position 1-2 and X12 is closed. The output current can vary from 0 to 100% of the maximum output current (in this evaluation board from 0 to 1 A). By removing the X12 jumper the output current will reach its maximum value. The PWM signal has to be applied as digital signal on X18 (max. 45 V). Jumpers are populated as follows:

Jumper number	Condition	Meaning
X9	Close 2-3	Disable CCSC
X10	Close 2-1	Disable battery dependent current
X12	Closed	Adjustable output current enabled

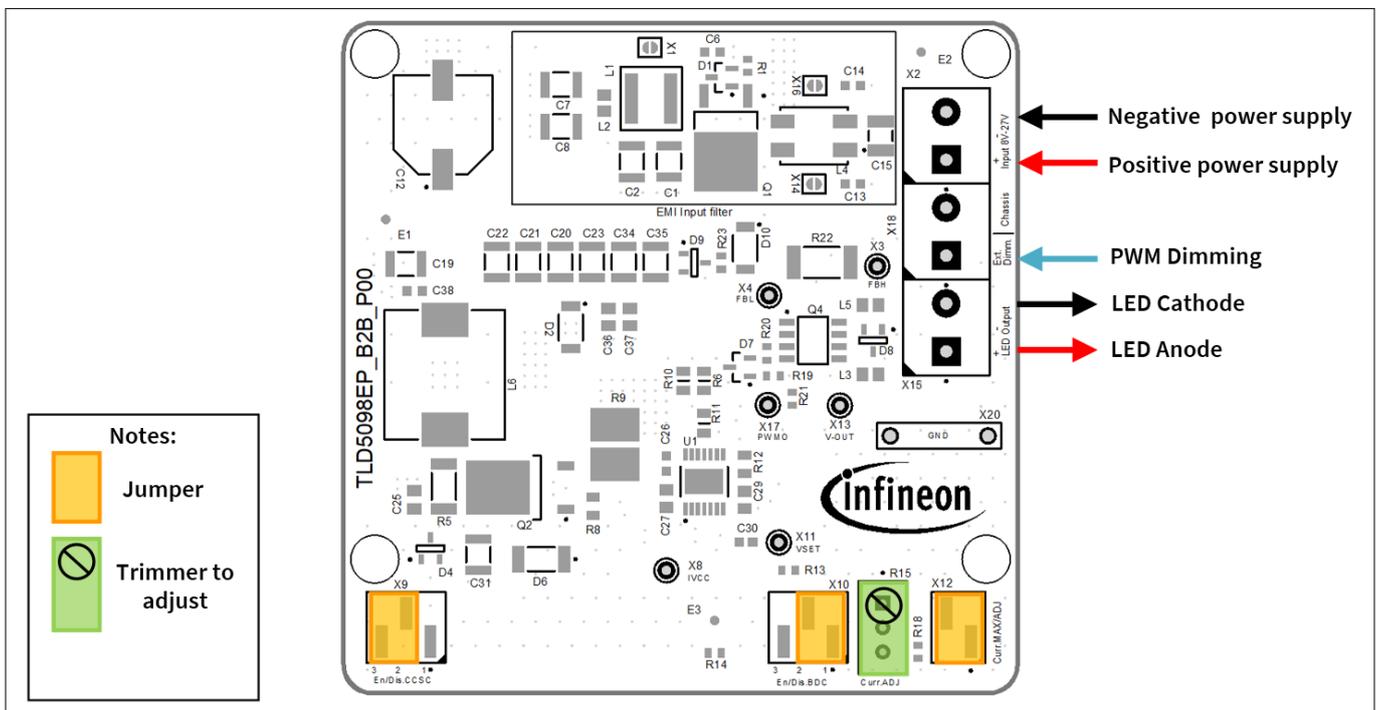


Figure 4 Current adjustment

4 Power derating (battery dependent current)

4 Power derating (battery dependent current)

The power derating acts by reducing V_{SET} (and thus the output current) when the battery voltage drops below 8 V. It works better when R15 is trimmed to its maximum value. Otherwise a different derating profile is applied. If a different derating profile is needed, R14 has to be changed. The aim is to have 1.6 V on pin SET when the battery voltage reaches the desired threshold, below which the output current must decrease proportionally. R14 can be calculated using:

(1)

$$R14 = (R15 + R18) \cdot \left(\frac{V_{BATT}}{1.6} - 1 \right)$$

where:

- R15 = 10 kΩ
- R18 = 560 Ω

For example, if the power derating should start when the battery voltage drops under 12 V, R14 must be replaced with a 68 kΩ 0603 resistor (please refer to the TLD5098EP datasheets for more information).

The PWM signal has to be applied as digital signal on X18 (max. 45 V).

Jumpers are populated as follows:

Jumper number	Condition	Meaning
X9	Close 2-3	Disable CCSC
X10	Close 2-3	Enable battery dependent current
X12	Closed	Adjustable output current enabled

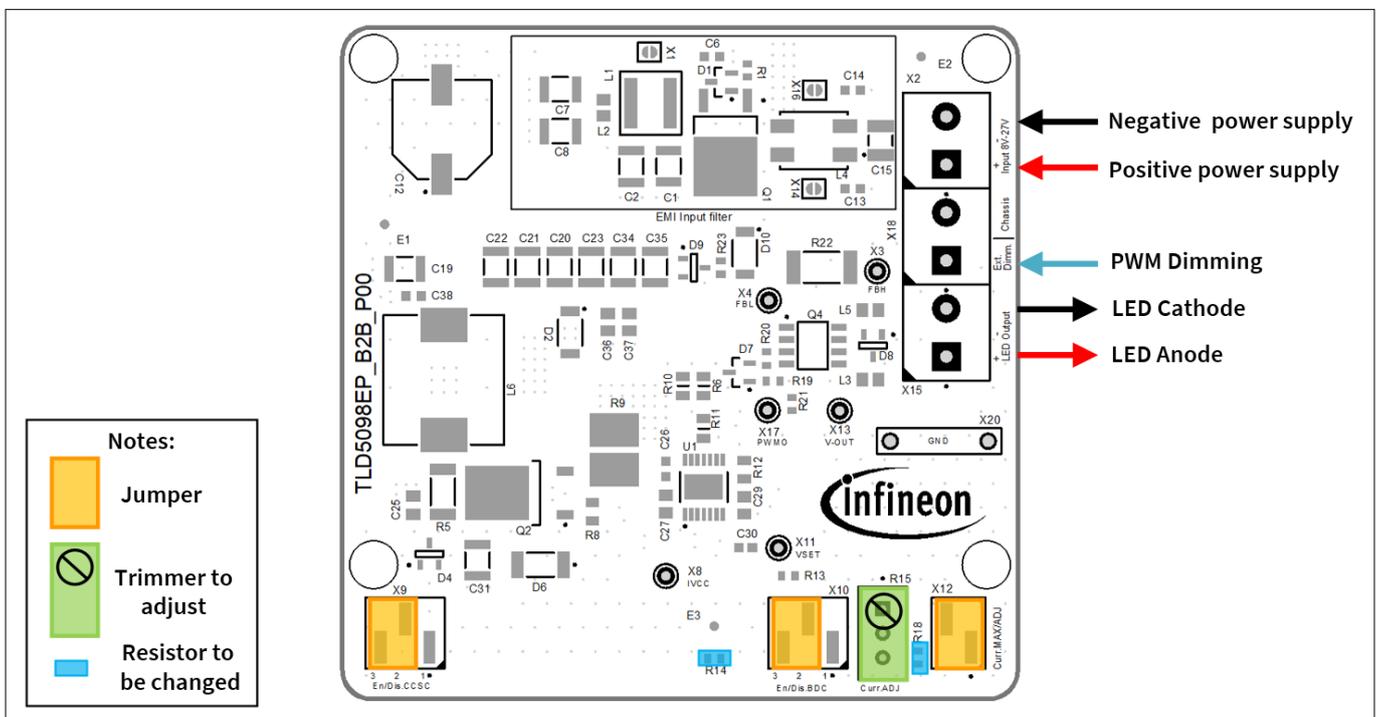


Figure 5 Power derating

5 Cold crank survival circuit

5 Cold crank survival circuit

This feature helps the system to survive LV124 test E11 "severe test pulse", when the input voltage drops below 4.5 V, which is the minimum input voltage for the TLD5098EP. This circuit feeds back the device with the output voltage when the input voltage drops. To activate this feature, close X9 in position 1-2. Other settings can be left as preferred.

Note: The CCSC uses a Zener diode to adapt the output voltage to the required voltage for the TLD5098EP, so that it can derate the efficiency performance.

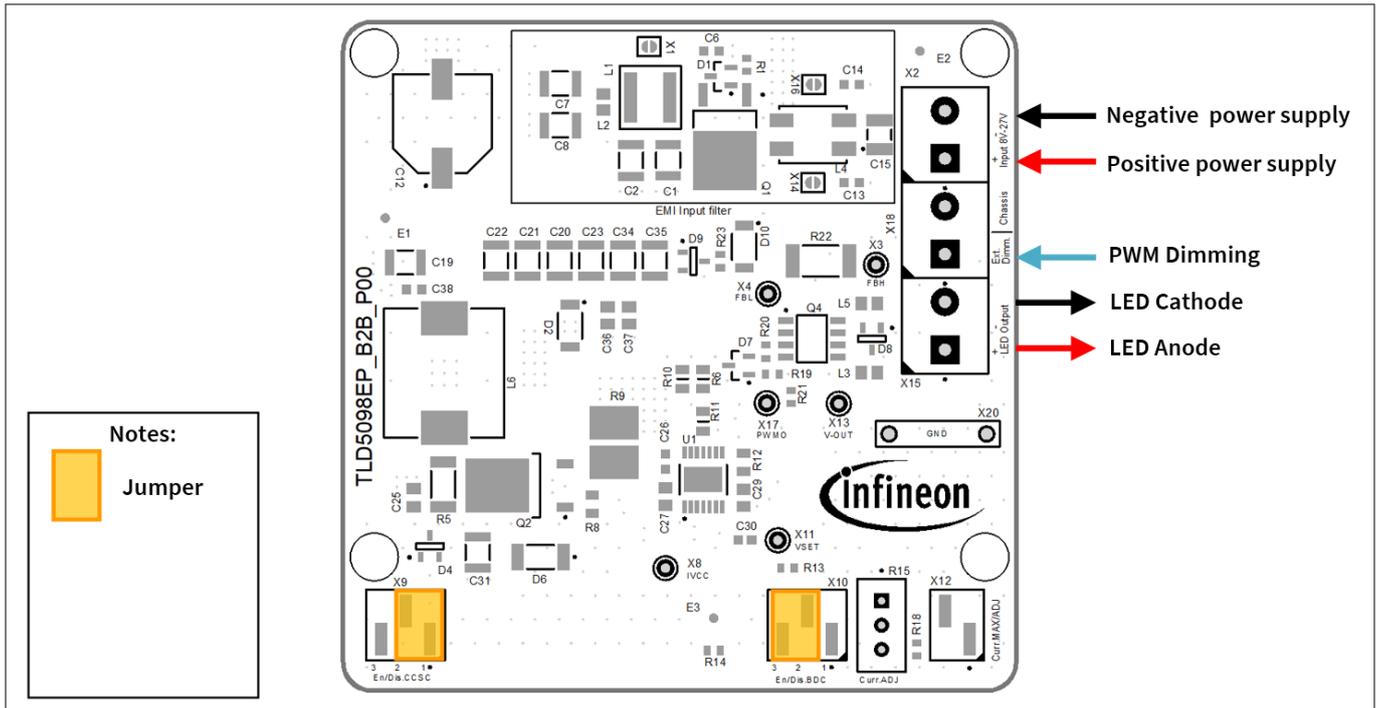


Figure 6 Cold crank survival circuit

7 PCB layout

7 PCB layout

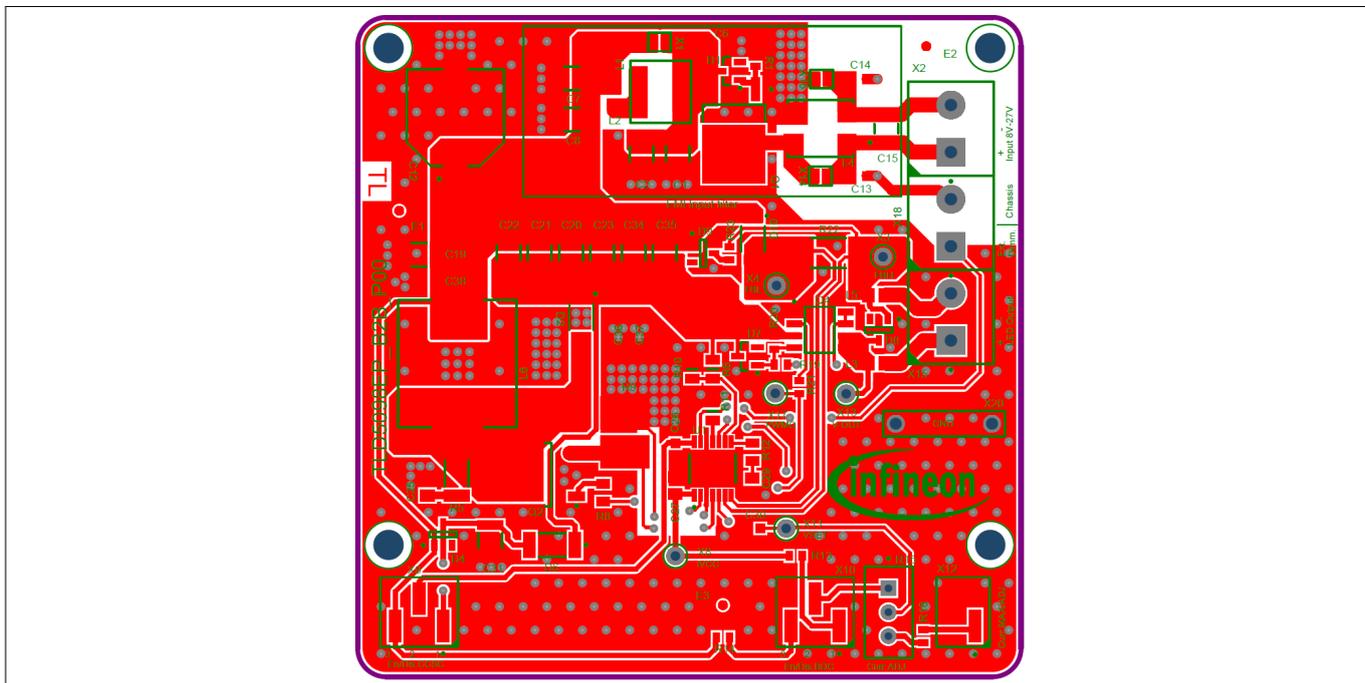


Figure 10 PCB layout top view

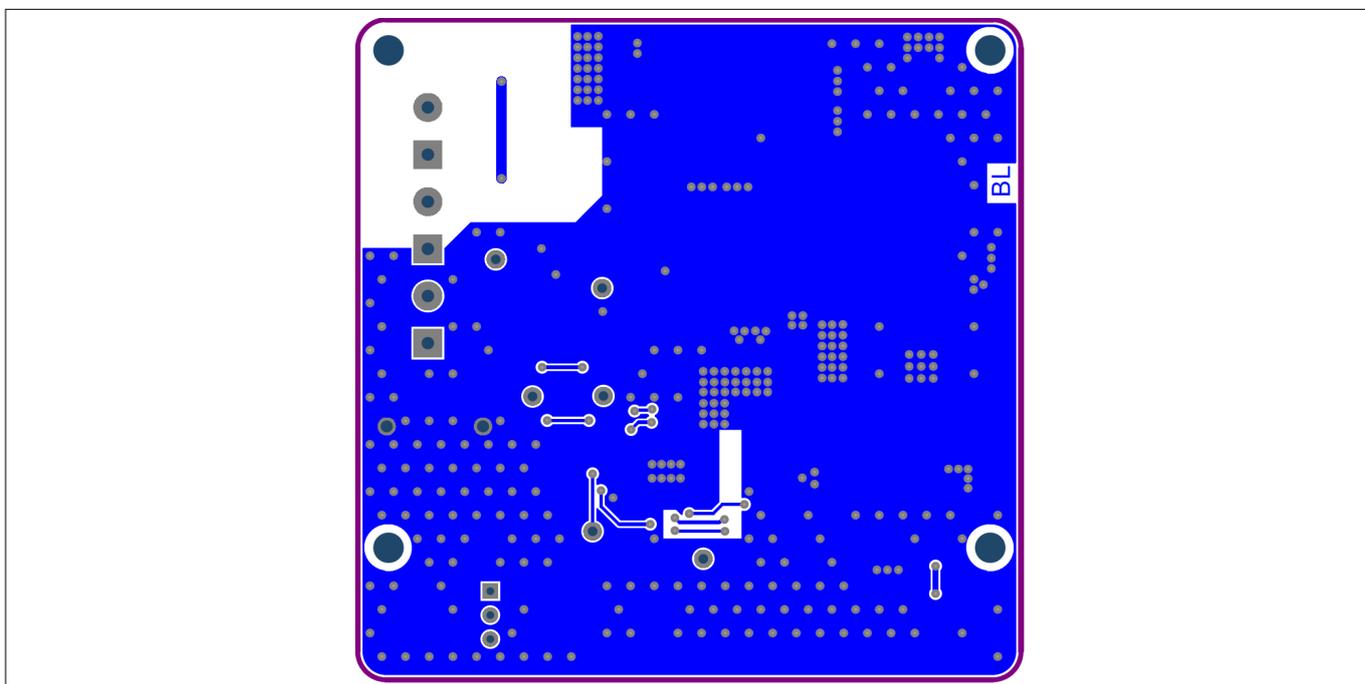


Figure 11 PCB layout bottom view

8 Bill of material

8 Bill of material

Table 2 Bill of material

Designator	Value	Manufacturer	Manufacturer order number
C1, C2, C7, C8, C19, C20, C21, C22, C23, C31, C34, C35	10 uF	Murata	GCM32EC71H106KA03
C6, C26, C38	100 nF	AVX	06035C104K4Z2A
C12	220 uF	Panasonic	EEEFK1H221P
C13, C14	470 pF	muRata	GCM1885C1H471JA16
C15	4.7 uF	Kemet	C1210C475K5RACAUTO
C25	1 nF	TDK Corporation	CGA4F2X7R2A102M085AE
C27	10 uF	TDK	CGA4J1X7S1C106K125AC
C29, C36	100 nF	TDK	CGA4J2X7R2A104M125AE
C30	1 uF	TDK	CGA3E1X7R1V105K080AC
C37	1 uF	TDK Corporation	CGA4J3X7S2A105K125AB
D1, D7	10 V	ON Semiconductor	BZX84C10LT1G
D2, D10	PMEG6030EP,115	Nexperia	PMEG6030EP,115
D4, D8, D9	BAS16	Infineon Technologies	BAS16
D6	10 V	Vishay	ZMY10-GS08
L1	10 uH	Coilcraft	XAL6060-103MEB
L2	100 Ω @ 100 MHz	TDK Corporation	MPZ2012S101ATD25
L3, L5	1 k Ω @ 100 MHz	TDK	MPZ2012S102ATD25
L4		TDK	ACM70V-701-2PL-TL00
L6	47 uH	Bourns	SRP1265A-470M
Q1	IPD90P04P4L-04	Infineon Technologies	IPD90P04P4L-04
Q2	IPD22N08S2L-50	Infineon Technologies	IPD22N08S2L-50
Q4	BSO615CGHUMA1	Infineon Technologies	BSO615CGHUMA1
R1, R23	10 k Ω	Vishay	CRCW060310K0FK
R5	2.2 Ω	Vishay	CRCW20102R20FK
R6	46.4 k Ω	Vishay	CRCW080546K4FK
R8, R12	0 Ω	Yageo	AC0805JR-070RL
R9	33 m Ω	Vishay	WSHM2818R0330FEA
R10	1 k Ω	Vishay	CRCW08051K00FK
R11	14 k Ω	Vishay	CRCW080514K0FK
R13, R20	22 k Ω	Vishay	CRCW060322K0FK
R14	39 k Ω	Vishay	CRCW060339K0FK
R15	10 k Ω	Vishay	T93YA103KT20
R18	560 Ω	Vishay	CRCW0603560RFK

8 Bill of material

Table 2 Bill of material (continued)

Designator	Value	Manufacturer	Manufacturer order number
R19	27 k Ω	Vishay	CRCW060327K0FK
R21	10 Ω	Vishay	CRCW060310R0FK
R22	300 m Ω	Vishay	WSL2512R3000FEA
U1	TLD5098EP	Infineon Technologies	TLD5098EP
X1, X14, X16	Solder Jumper 2 Pins		Solder Jumper 2 Pins
X2, X15, X18	1935776	Phoenix Contact	1935776
X3, X4, X8, X11, X13, X17	5001	Keystone	5001
X9, X10	TSM-103-01-S-SV	Samtec	TSM-103-01-S-SV
X12	TSM-102-01-S-SV	Samtec	TSM-102-01-S-SV
X20	D3082-05	Harwin	D3082-05

9 Efficiency measurements

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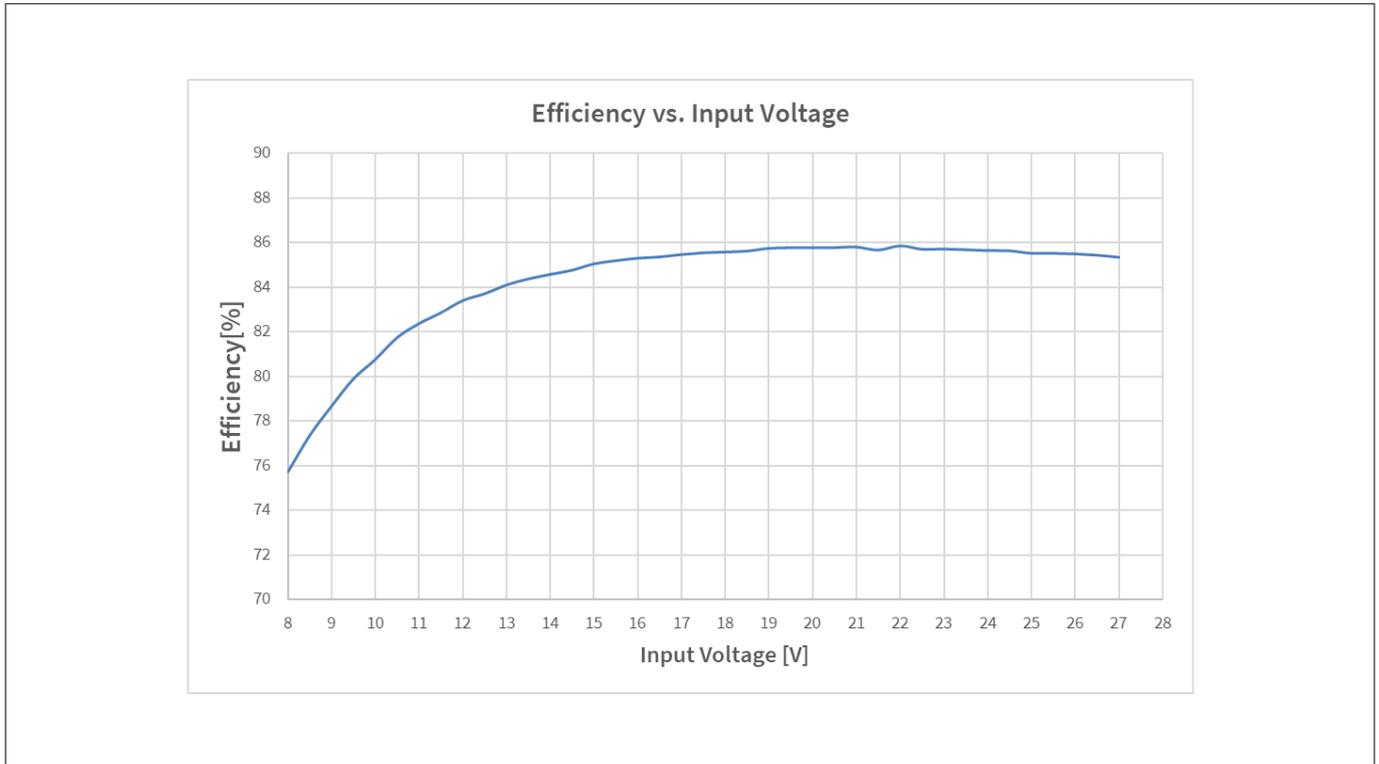


Figure 12 Efficiency vs. input voltage

This efficiency performance has been obtained with:

Table 3 Parameters influencing efficiency

Output load:	Series of 7 white standard LEDs with $V_J \sim 3\text{ V}$ kept cooled with forced air
EMI filter:	Totally bypassed by closing the jumpers X1, X14 and X16
CCSC:	Off (jumper X9 closed on 2-3)
Current adjustment:	Off (jumper X12 left open)
Dimming:	100% D.C.
Power derating:	Off (jumper X10 closed on 1-2)

Efficiency performances can be increased, see [Chapter 11](#).

10 Maximizing efficiency

10 Maximizing efficiency

This evaluation board has been designed to reach a fair compromise between efficiency performance and EM emissions compliance.

Nevertheless, if the maximum efficiency is needed, the following actions should be considered:

1. Remove the snubber circuit consisting of R5 and C25, or choose a lower value for the capacitor C25 (for example 470 pF)
2. Bypass the whole EMI filter by bridging the jumpers X1, X14 and X16
3. Bypass the output ferrite beads L3 and L5
4. Replace the main inductor L6 with one that boasts a lower parasitic DC resistance, for example
 - Vishay IHLP6767GZER470M8A
 - Bourns SRP1770TA-470M
5. Turn off the CCSC by placing the jumper X9 on position 2-3

11 Minimizing EM emissions

11 Minimizing EM emissions

This evaluation board has been designed to reach a fair compromise between efficiency performance and conducted EM emissions compliance from 150 kHz to 108 MHz.

Nevertheless, if the minimum EM emission is required, the following actions should be considered:

- 1.** Choose a higher value for the capacitor C25 (for example 2.2 nF)
- 2.** Include the whole EMI filter by removing bridges from the jumpers X1, X14 and X16
- 3.** Replace the 0 Ω resistor R8 with a small value such as 10 Ω or 22 Ω
- 4.** Replace the main inductor L6 with a shielded one (for example Cynotec VCHE106G-470MS6) and connect the shield to ground
- 5.** Connect the CHASSIS terminal with a short piece of wire as close as possible to the test ground plane where the board is placed

12 Revision history

12 Revision history

Document version	Date of release	Description of changes
Rev. 1.00	2020-09-17	First release related to evalboard S00_P00

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